

## Precise equatorial coordinates of double and multiple systems: an astronomical support to the Hipparcos mission

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**Abstract.** — In this work we report on the determination of precise positions of 623 double and multiple stars (126 of which are newly discovered systems) obtained from the measurement of 39 plates taken at both the European Southern Observatory (ESO) and the Astronomical Observatory of Torino (AOT) during the period 1984-87. Those positions will be used to update the *Catalogue de Composantes d'étoiles Doubles et Multiples (CCDM)* and, consequently, the Input Catalogue of the Hipparcos mission, as the CCDM, established on the basis of the Index (1976,5), is the reference source for the known double and multiple stars that appear on the Hipparcos list. Several visual doubles on the list presented here are within those included in the final observing program of the Hipparcos astrometric mission.

**Key words:** double stars — multiple systems — Hipparcos mission

### 1. Introduction.

The space astrometry mission Hipparcos started back in the late summer of 1989. The main goal of this mission is the accurate determination of position, parallax and proper motion of about 120 000 stars with blue magnitude brighter than 13.

About 14 000 of the program stars are known double and multiple systems. Observations of these stars (as well as the other stars in the program) and their subsequent successful reduction require that the absolute position of each component be known at the 1 arcsec level (per coordinate). This astrometric necessity imposed by the Hipparcos mission, along with the unsatisfactory precision of most of the existing data, has called for new observation campaigns leading to the creation of a new catalogue of double and multiple stars. This is the CCDM catalogue, established on the basis of the Index (1976,5) (upgrade of the Index Catalogue of Jeffers and van den Bos, 1963) and completed at the Royal Observatory, Belgium. This catalogue has been the main source list of double and multiple star positions while preparing the Input Catalogue for the Hipparcos mission (Turon 1989).

Given the improved nature of the positions listed in the CCDM, this catalogue will also be quite useful during the reduction of the Hipparcos data taken on double and multiple systems. As good provisional data are needed for

the successful extraction of the astrometric parameters of non-single stars, the CCDM will serve as the main data base for the retrieval of those preliminary data.

The main goal of this work is to provide positions of a set of double and multiple stars listed in the CCDM to the accuracy required for their possible inclusion in the Hipparcos Input Catalogue.

### 2. Instrumentation, observations, and data reduction.

All the results reported in this paper refer to two sets of observations carried out at the European Southern Observatory (ESO) and at the Astronomical Observatory of Torino (AOT). More precisely, 27 plates were exposed using the 386/3994 mm astrograph (GPO) of the ESO Observatory at La Silla (Chile) over the period 1984-87, while 12 plates were obtained at the AOT during the period 1985-87 with the 380/6875 mm photographic refractor. Kodak IIa-O spectroscopic plates (16 cm on a side) were usually used at both Observatories. The number of exposures on each plate are usually 3 for the AOT plates and 1 for the ESO plates. Each image was measured twice with either a semi-automatic or a manual Ascorecord measuring machine (both machines are available at the AOT).

The equatorial coordinates of the reference stars were selected from the AGK3 catalogue (Heckmann and Dieckvoss 1975) when the declination of the targets was above

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$-2^\circ$ , while the SAO catalogue was used for declinations below this value.

All the plates used in this study were reduced via a least squares adjustment to a standard 6-constant plate model (Eichhorn 1974). The derived equatorial coordinates, in the B1950.0 system (as defined by the AGK3 or the SAO catalogues), were reduced to the J2000.0 system using the procedure of Aoki *et al.* (1983). The polar coordinates of the binary and multiple stars ( $\rho$  and  $\theta$ ) have been derived from the computed equatorial coordinates of each component in the systems. Consequently, the orientations of these systems refer to the North Pole of the J2000.0 system.

126 new systems have been discovered and measured. These new systems are named as AOT followed by a progressive number in Table 1.

We have also derived magnitude estimates for those new systems (for the others we always used the CCDM values). As both the ESO and the AOT plates used blue sensitive emulsions and were taken without any filter, those magnitudes are in the photographic (mpg) system. We found four GPO plates partially overlapped with four Southern Selected Areas (Brun & Vehreberg 1980). The magnitudes of the double and multiple stars found on these four plates were then visually estimated using the stars in the Selected Areas compilation as comparisons. For the other ESO plates, the magnitudes were estimated by comparison with the previous four plates, after taking into account the difference in exposure time.

As for the Torino plates, no comparison stars from any Selected Areas field were available. The estimates were made using a M 44 (Praesepe) blue plate, exposed through the same instrument, and developed and processed following the same procedure used for the present plates. This plate thus sets the magnitude scale for the estimation of the unknown magnitudes. The magnitude zero-point was fixed using those AGK3 or SAO stars available on the plates.

Some internal check were made to avoid large plate to plate systematic errors. No differences greater than 0.2–0.3 mag were found.

### 3. Results.

In Table 1 the equatorial positions of 623 components of double and multiple stars or the photocenters of the unresolved systems. There are 20 components of multiple systems with entries in the CCDM but without position in Table 1 as they were either not visible on the plates or unmeasurable, and 25 couples of multiple systems of which the polar coordinates are given while the absolute position is the same of the preceding entry.

More precisely, the columns of Table 1 are as follows:

- 1: Index number (based on the position at the reference epoch 1900.0) according to the CCDM designation.
- 2: Name of the discoverer; binaries with the designation AOT are new systems not previously catalogued.
- 3: Binary component according to the CCDM designation (A = main component, B = the secondary one, C = the third one, and so on). When 2 letters shifted to the right appear in this column (e.g. AB, BC, etc...), it means that the 2 components are so closed that only the photocenter was measured. When 2 letters shifted to the left appear, it means that the listed absolute position is that of the secondary component (letter), while the position relative to the primary is that of the couple.
- 4: Magnitude of the components as given in the CCDM catalogue. For the newly discovered systems (AOT designation) a magnitude estimate is provided (see section 2 above).
- 5: Epoch of observation without the initial 2 digits.
- 6: Right Ascension referred to the J2000.0 equinox.
- 7: Declination, as before.
- 8: Position angle referred to the J2000.0 North Pole (in degrees).
- 9: Angular separation (in arcsec).
- 10: DM number (Durchmusterungen Catalogues BD and CD). For some of the newly discovered systems the DM number (BD or CD) has been computed and inserted here.
- 11: ADS number.
- 12: Number of the plate containing the system and Observatory where that plate was taken, 1: AOT, 2: ESO.
- 13: Component without positions: NM = Not Measured, NS = Not Seen.

### 4. Discussion.

Given the requirements imposed by the Hipparcos mission recalled in the Introduction, we will discuss here the accuracy of the results reported in Table 1. The assessment is based on the statistics of the (O-C) residuals of the reference stars (used during the plate reductions) both in Right Ascension and Declination.

In Table 2 we report the results for all the 39 plates used in this study. They have been divided into four different groups according to the Observatory of origin (AOT or ESO) and to the reference catalogue used with them (SAO or AGK3).

Then, Table 2 shows the following plate groups:

- a) 10 AOT plates reduced with the AGK3,
- b) 2 AOT plates reduced with the SAO,
- c) 25 ESO plates reduced with the SAO,
- d) 2 ESO plates reduced with the AGK3.

The columns of the table have the following meaning:

TABLE 2.

1	2	3	4	5	6	7
				"	"	"
945	(1)	AGK3	18	0.35	0.20	0.40
946	(1)	AGK3	13	0.34	0.27	0.43
947	(1)	AGK3	10	0.41	0.41	0.58
948	(1)	AGK3	9	0.66	0.43	0.79
949	(1)	AGK3	12	0.36	0.25	0.44
950	(1)	AGK3	13	0.27	0.59	0.65
955	(1)	AGK3	12	0.45	0.28	0.53
996	(1)	AGK3	8	0.50	0.50	0.71
1000	(1)	AGK3	9	0.38	0.66	0.76
1003	(1)	AGK3	6	0.52	0.48	0.71
Weighted mean - group a				0.40	0.38	0.57
				"	"	"
1001	(1)	SAO	8	0.72	1.11	1.32
1002	(1)	SAO	6	0.85	0.65	1.07
Weighted mean - group b				0.78	0.91	1.21
				"	"	"
7676	(2)	SAO	16	1.02	0.56	1.16
7682	(2)	SAO	12	1.27	1.65	2.08
11131	(2)	SAO	14	0.73	0.95	1.20
11134	(2)	SAO	11	0.53	0.75	0.92
11138	(2)	SAO	13	0.58	0.54	0.79
11143	(2)	SAO	15	1.10	0.71	1.31
11149	(2)	SAO	10	0.62	0.25	0.67
11151	(2)	SAO	12	0.99	0.85	1.30
11157	(2)	SAO	9	0.74	0.72	1.03
11158	(2)	SAO	13	0.88	0.91	1.27
11160	(2)	SAO	16	0.72	0.92	1.17
11171	(2)	SAO	13	0.80	0.46	0.92
11174	(2)	SAO	13	0.72	1.00	1.23
11175	(2)	SAO	17	0.74	0.68	1.00
11177	(2)	SAO	8	1.25	0.83	1.50
11199	(2)	SAO	7	0.43	0.77	0.88
11209	(2)	SAO	7	0.98	1.07	1.45
11210	(2)	SAO	8	0.73	0.59	0.94
11222	(2)	SAO	11	0.68	1.00	1.21
11224	(2)	SAO	8	0.53	0.78	0.94
11234	(2)	SAO	9	0.65	0.45	0.79
11239	(2)	SAO	9	0.74	0.46	0.87
11272	(2)	SAO	7	0.58	0.89	1.06
11273	(2)	SAO	9	0.85	0.58	1.03
11274	(2)	SAO	9	0.73	1.06	1.29
Weighted mean - group c				0.80	0.78	1.13
				"	"	"
11176	(2)	AGK3	17	0.63	0.61	0.88
11211	(2)	AGK3	18	0.54	0.52	0.75
Weighted mean - group d				0.58	0.56	0.81

- 1: Plate number.
- 2: Observatory Identification number (1): AOT, (2): ESO.
- 3: Reference Catalogue used.
- 4: Number of reference stars used in the plate solution.
- 5: Mean error of unit weight in Right Ascension as computed from (O-C) residuals (arcsec).
- 6: The same as column 5 for Declination (arcsec).

7: Total mean error of unit weight computed as the square root of the sum of the squares of the values in columns 5 and 6 (arcsec).

Under each group of plates, separated by a dashed line, we give the weighted mean values of the data reported in Columns 5, 6 and 7. As weights, we have used the number of reference stars in column 4.

The average results in Table 2 indicate good agreement between Right Ascension and Declination. Also, the precision of the positions of group *a* is twice as good as that of group *c*. This is not surprising as the AGK3 is such a better catalogue than the SAO, and it seems to indicate that the different scale of the two telescopes used does not play any significant role as the error budget for the ESO plates is dominated by the SAO errors. Evidence that this is indeed the case can be inferred by comparing set *a* to set *d* and set *b* to set *c*. Although statistics is poor for the two smaller groups and caution must be paid in deriving any conclusive argument, it appears that the increased error of group *d* as compared to group *a* is almost entirely accounted for by the more favourable scale of the AOT refractor. The same effect does not show when comparing the corresponding groups *b* and *c*.

As very similar machines were used to measure the plates and the same plate model adopted during the reductions, the fact that the average precision of sets *a* and *d* scales nicely with the different plate scale indicates that the GPO astrograph and the AOT refractor have quite similar astrometric properties.

Further evidence of the dominant role of the SAO catalogue in determining the final precision of most of the ESO plates is given in Fig. 1.

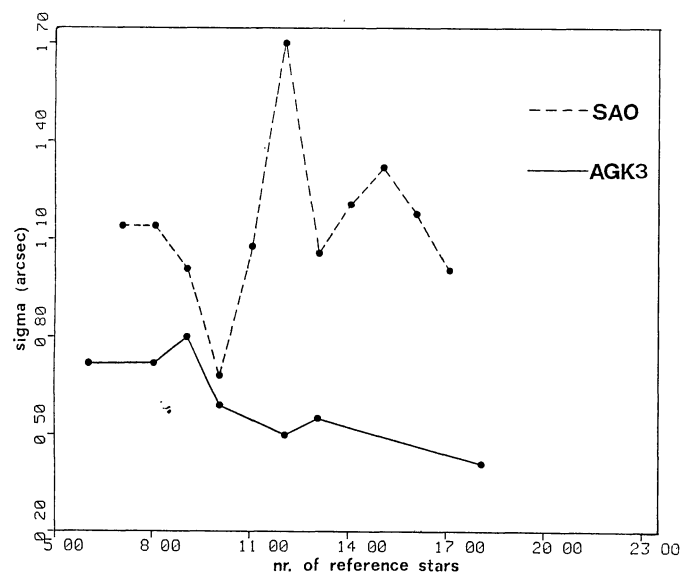


FIGURE 1. Number of reference stars against standard deviation for the SAO and AGK3 stars

Here the total (positional) error of unit weight (column 7 in Table 2) is plot versus the number of reference stars used in the plate reductions (average values are used when two or more plates were reduced with the given number of reference stars) and for both the AGK3 and the SAO catalogues. The AGK3 curve clearly shows that the overall precision is improving with the number of reference stars as expected. Also, this curve appears to approach the value of 0.5 arcsec, which is quite consistent with an estimation of the AGK3 total precision at the mean epoch of our plates (1986.2) as derived using the data in de Vegt and Zacharias (1987). The SAO curve shows indeed a very different case. There is no evident benefit in using larger numbers of SAO stars, which seems to indicate the presence of inconsistencies in the reference catalogue itself. This would not be too much of a surprise given that the SAO catalogue is a compilation resulting from the merging of many different (and inhomogeneous) source catalogues (SAO staff 1966). From the introduction to the SAO catalogue we expected a total (position) error of about 0.6 arcsec at the epoch of the plates. From Fig. 1, we infer a much different value of about 1.2 arcsec, which is in fair agreement with the findings presented in Table 2 of Taff et al. (1990).

The previous analysis supports the interpretation that the AGK3 or SAO catalogue errors at the epoch of the plates contribute most of the unit weight errors listed in Table 2. Thus, the precision (at least relative) of the positions given in this work is well within the requirement imposed by the Hipparcos mission for their acceptance in the CCDM catalogue and, consequently, in the Hipparcos Input Catalogue.

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TABLE 1.

1	2	3	4	5	6	7	8	9	10	11	12	13
					h m s	° ' "	°	"				
01151S1720		A	11.0		87.88 01 19 59.763	-16 48 09.73						1001 1
01151S1720	AOT 1	B	12.8		87.88 01 19 58.330	-16 47 50.70	312.74	28.029				1001 1
01166S1700	HU 417	AB	10.0 13.2		87.88 01 21 31.643	-16 28 58.27			-17 239 1100			1001 1
01175S1723		A	11.2		87.88 01 22 21.649	-16 51 38.31						1001 1
01175S1723	AOT 2	B	13.5		87.88 01 22 21.642	-16 51 54.66	180.36	16.355				1001 1
01188S1702		A	10.5		87.88 01 23 41.065	-16 31 03.11						1001 1
01188S1702	AOT 3	B	13.3		87.88 01 23 40.439	-16 31 09.82	233.31	11.229				1001 1
01467S1714		A	9.0		87.88 01 51 28.478	-16 44 24.41			-17 330			1002 1
01467S1714	AOT 4	B	13.3		87.88 01 51 28.921	-16 44 32.42	141.55	10.227				1002 1
01483S1713	BU 183	AB	8.9 9.9		87.88 01 53 07.956	-16 43 57.81			-17 340 1505			1002 1
02155S0847		A	9.5		87.59 02 20 23.256	-08 19 11.59			-08 426			11210 2
02155S0847	AOT 5	B	12.9		87.59 02 20 23.543	-08 19 25.67	163.13	14.703				11210 2
02177S0756		A	12.6		87.59 02 22 40.682	-07 28 43.31						11210 2
02177S0756	AOT 6	B	14.4		87.59 02 22 40.389	-07 29 00.77	194.02	17.996				11210 2
02184S0817		AB	9.3 9.7		87.59 02 23 17.496	-07 49 04.75			-08 435 1821			11210 2
02184S0817	HO 313	C	13.4		87.59 02 23 18.628	-07 49 01.38	78.67	17.154			1821	11210 2
02191S0819		A	9.6		87.59 02 24 01.013	-07 51 46.28			-08 438 1828			11210 2
02191S0819	HO 314	B	11.4		87.59 02 24 00.831	-07 51 50.95	210.01	5.391	-08 438 1828			11210 2
02191S0819	HO 314	C	12.0		87.59				-08 438 1828			11210 2 NM











TABLE 1 (continued)

18056S1808	ARA 457	B	12.8		87.59	18	11	28.390	-18	06	35.44	2.55	14.115			11174	2	
18059S1826		A	10.2		87.59	18	11	46.723	-18	22	52.31			-18	4826	11136	11174	2
18059S1826	HJ 2820	B	11.4		87.59	18	11	46.281	-18	22	51.21	279.97	6.384			11136	11174	2
18059S1826	HJ 2820	C	11.5		87.59	18	11	47.605	-18	22	50.06	79.81	12.763	-18	4286	11136	11174	2
18059S1826		BC			87.59	18	11	47.605	-18	22	50.06	86.50	18.885			11136	11174	2
18061S1542	HO 429	AB	8.1	12.0	87.59	18	11	50.979	-15	40	47.74			-15	4856	11140	11175	2
18066S1549		A	11.0		87.59	18	12	20.575	-15	48	12.73						11175	2
18066S1549	BRT 586	B	11.2		87.59	18	12	20.229	-15	48	13.85	77.35	5.108				11175	2
18067S1524	LV 7	AB	8.0	11.6	87.59	18	12	28.510	-15	22	23.73			-15	4864	11146	11175	2
18067S1524	LV 7	C	11.6		87.59											11146	11175	2
18067S1524	AO7 71	D	14.0		87.59	18	12	29.096	-15	22	40.28	152.90	18.588				11175	2
18070S1619		A	10.2		87.59	18	12	48.547	-16	17	46.56			-16	4755	11151	11175	2
18070S1619	HJ 2821	B	10.6		87.59	18	12	47.974	-16	17	45.17	279.53	8.367			11151	11175	2
18073S1538		A	9.8		87.59	18	13	03.559	-15	35	50.48						11175	2
18073S1538	J 2200	B	10.5		87.59	18	13	03.207	-15	35	56.41	220.63	7.812				11175	2
18078S1537	BU 131	AB	7.3	9.3	87.59	18	13	35.531	-15	35	54.04			-15	4874	11166	11175	2
18078S1537		C	11.5		87.59	18	13	34.947	-15	35	50.00	295.58	9.349			11166	11175	2
18078S1537		D	12.0		87.59											11166	11175	2
18085S1633		A	9.3		87.59	18	14	20.876	-16	32	11.81						11175	2
18085S1633	J 1648	B	11.8		87.59	18	14	21.311	-16	32	11.88	90.63	6.260				11175	2
18096S1624		A	9.7		87.59	18	15	25.462	-16	22	56.92						11175	2
18096S1624	J 1649	B	10.8		87.59	18	15	25.373	-16	22	53.60	338.83	3.559				11175	2
18099S1604		A	10.8		87.59	18	15	37.765	-16	01	42.63						11175	2
18099S1604	AO7 72	B	13.2		87.59	18	15	37.652	-16	01	34.09	349.17	8.687				11175	2
18101S1556	RST4005	AB	9.9	11.7	87.59	18	15	50.639	-15	53	58.88			-15	4897		11175	2
18102S1507		A	9.3		87.59	18	15	57.033	-15	06	17.00			-15	4895		11175	2
18102S1507	J 2202	B	11.0		87.59	18	15	57.034	-15	06	25.34	179.83	8.332				11175	2
18106S1508		A	9.3		87.59	18	16	18.810	-15	07	19.43						11175	2
18106S1508	J 2203	B	12.0		87.59	18	16	19.788	-15	07	19.20	89.08	14.153				11175	2
18106S1508	J 2203	C	13.0		87.59												11175	2
18109S1453		A	11.7		87.59	18	16	34.136	-14	51	02.81						11175	2
18109S1453	BRT 587	B	11.8		87.59	18	16	34.070	-14	51	00.54	337.22	2.463				11175	2
18120S1614		A	10.4		87.59	18	17	44.410	-16	11	29.90			-16	4798		11175	2
18120S1614	ARA 102	B	12.5		87.59	18	17	45.135	-16	11	30.36	92.50	10.458				11175	2
18380S0125		A	12.2		87.59	18	43	10.984	-01	19	30.96						11176	2
18380S0125	AO7 73	B	12.7		87.59	18	43	10.519	-01	19	21.79	322.79	11.524				11176	2
18386S0020	A 858	AB	9.0	14.0	87.59	18	43	43.482	-00	14	10.84			-00	3539	11613	11176	2
18386S0020	AO7 74	C	13.8		87.59	18	43	42.009	-00	13	57.71	300.75	25.697				11176	2
18388S0019	A 859	AB	8.5	8.9	87.59	18	43	53.675	-00	13	27.08			-00	3540	11614	11176	2
18395S0106		A	9.5		87.59	18	44	39.618	-00	59	44.24			-01	3556		11176	2
18395S0106	HJ 5501	B	10.8		87.59	18	44	39.761	-00	59	22.31	5.59	22.035				11176	2
18400N3912		A	6.6		85.48	18	43	16.600	+39	18	00.55			+39	3505		945	1
18400N3912	BUP	B	10.4		85.48	18	43	15.554	+39	17	00.72	191.47	61.050	+39	3504		945	1
18405S0113		A	9.5		87.59	18	45	41.212	-01	06	50.69						11176	2
18405S0113	BAL 582	B	11.0		87.59	18	45	40.729	-01	06	40.97	323.25	12.123				11176	2
18413S0104		A	6.1		87.59	18	46	28.645	-00	57	41.27			-01	3559	11667	11176	2
18413S0104	STF2379	B	7.9		87.59	18	46	29.403	-00	57	48.63	122.93	13.542			11667	11176	2
18413S0104	STF2379	C	11.3		87.59	18	46	29.486	-00	58	01.82	148.45	24.116			11667	11176	2
18413S0104		BC			87.59	18	46	29.486	-00	58	01.82	174.57	13.249			11667	11176	2
18414S0155	RST5125	AB	10.7	11.0	87.59	18	46	34.542	-01	48	50.19			-01	3560		11176	2
18418N3907		A	8.4		85.48	18	45	10.016	+39	13	32.44			+39	3517	11655	945	1
18418N3907	STF2392	B	10.4		85.48	18	45	09.817	+39	13	35.27	320.83	3.657			11655	945	1
18418N3907	STF2392	C	9.6		85.48	18	45	10.264	+39	13	09.22	172.92	23.396	+39	3517	11655	945	1
18418N3907		BC			85.48	18	45	10.264	+39	13	09.22	168.73	26.565			11655	945	1
18418N3813		A	7.7		85.48	18	45	10.874	+38	18	54.79			+38	3280	11656	945	1
18418N3813	STF2393	B	10.4		85.48	18	45	11.433	+38	19	10.09	23.26	16.657			11656	945	1
18418N3813	STF2393	C	11.3		85.48	18	44	57.567	+38	20	29.14	301.07	182.841			11656	945	1
18418N3813		BC			85.48	18	44	57.567	+38	20	29.14	295.85	181.321			11656	945	1
18432N3815	HU 1191	AB	8.6	9.1	85.48	18	46	34.604	+38	21	04.32			+38	3292	11680	945	1
18432N3846		A	10.3		85.48	18	46	37.281	+38	52	24.17			+38	3294	11679	945	1
18432N3846	ES 2021	B	11.2		85.48	18	46	35.574	+38	52	18.09	253.04	20.843			11679	945	1
18432N3846	ES 2021	C	12.4		85.48	18	46	35.362	+38	52	19.24	257.57	22.944			11679	945	1
18432N3846		BC			85.48	18	46	35.362	+38	52	19.24	294.83	2.722			11679	945	1
18432S0122		A	10.4		87.59	18	48	20.601	-01	14	46.29						11176	2
18432S0122	BAL 584	B	11.0		87.59	18	48	20.119	-01	14	55.75	217.38	11.902				11176	2
18436S0127		A	9.8		87.59	18	48	47.830	-01	20	40.25						11176	2
18436S0127	BAL 585	B	10.1		87.59	18	48	47.983	-01	20	44.31	150.50	4.669				11176	2
18446N3851		A	10.0		85.48	18	47	59.811	+38	57	57.35						945	1
18446N3851	ES 2572	B	11.5		85.48	18	48	00.295	+38	58	00.06	64.42	6.256				945	1
18537N1206		A	9.6		85.48	18	58	13.840	+12	13	38.84						946	1
18537N1206	J 2537	B	11.9		85.48	18	58	13.886	+12	13	42.59	9.99	3.814				946	1
18540N1233		A	8.8		85.48	18	58	38.296	+12	41	32.79			+12	3742	11892	946	1
18540N1233	AG	B	9.6		85.48	18	58	38.032	+12	41	29.02	225.71	5.396			11892	946	1
18541N1209		A	10.6		85.48	18	58	40.099	+12	16	02.78			+12	3743		946	1
18541N1209	J 2581	B	13.2		85.48	18	58	39.702	+12	16	08.20	312.93	7.958				946	1
18553N1244		A	7.4		85.48	18	59	58.782	+12	53	24.91			+12	3750	11916	946	1
18553N1244	STF2426	B	8.8		85.48	18	59	57.638	+12	53	21.84	259.59	17.001			11916	946	1



TABLE 1 (continued)

19458N3751	ALI 634	B	13.3	85.56	19	49	26.118	+38	05	54.07	53.89	5.021		950	1		
19459N3828		A	6.2	85.56	19	49	27.506	+38	42	36.76			+38 3772	12992	950	1	
19459N3828	ES 84	B	11.1	85.56	19	49	27.814	+38	42	26.14	161.24	11.217		12992	950	1	
19459N3828	ES 84	C	11.2	85.56	19	49	29.427	+38	42	34.72	95.19	22.574		12992	950	1	
19459N3828		BC		85.56	19	49	29.427	+38	42	34.72	65.56	20.733		12992	950	1	
19465N3817		A	10.5	85.56	19	50	06.812	+38	32	39.97					950	1	
19465N3817	MLB 766	B	10.6	85.56	19	50	06.714	+38	32	46.37	349.79	6.500			950	1	
19470N3828		A	5.4	85.56	19	50	34.000	+38	43	18.98			+38 3780	13014	950	1	
19470N3828	HJ 603	B	10.4	85.56	19	50	38.426	+38	42	57.99	112.06	55.889		13014	950	1	
19470N3828	HJ 603	C	11.1	85.56	19	50	38.831	+38	43	18.45	90.54	56.540		13014	950	1	
19470N3828		BC		85.56	19	50	38.831	+38	43	18.45	13.05	20.995		13014	950	1	
19474N3855	A 1406	AB	9.2 11.8	85.56	19	50	56.888	+39	10	11.07			+38 3784	13021	950	1	
19477N3814		A	11.8	85.56	19	51	15.699	+38	29	43.22					950	1	
19477N3814	ALI 903	B	12.8	85.56	19	51	15.405	+38	29	34.96	202.70	8.945			950	1	
19482N3800		A	11.9	85.56	19	51	45.813	+38	15	51.08					950	1	
19482N3800	ALI 904	B	12.6	85.56	19	51	46.699	+38	15	47.67	108.08	10.977			950	1	
20264S4136		A	13.6	87.59	20	33	03.648	-41	16	10.90					11157	2	
20264S4136	BRT1111	B	13.9	87.59	20	33	03.757	-41	16	15.02	163.42	4.299			11157	2	
20277S4241	DON 988	AB	10.1 11.5	87.59	20	34	25.620	-42	20	10.66			-42 14972		11157	2	
20277S4241		C	9.7	87.59	20	34	23.536	-42	20	11.21	88.64	23.117		-42 14974		11157	2
20280S4304		A	11.7	87.59	20	34	45.091	-42	43	35.67				-43 14063		11157	2
20280S4304	AOT 80	B	14.2	87.59	20	34	44.151	-42	43	40.06	247.04	11.250			11157	2	
20283S4246		A	11.6	87.59	20	35	03.189	-42	25	47.70				-42 14978		11157	2
20283S4246	AOT 81	B	13.9	87.59	20	35	02.957	-42	26	01.96	190.19	14.491			11157	2	
20287S4301		A	11.7	87.59	20	35	29.558	-42	40	45.29				-43 14072		11157	2
20287S4301	AOT 82	B	14.0	87.59	20	35	29.445	-42	40	49.02	198.50	3.937			11157	2	
20289S4304		A	12.1	87.59	20	35	37.798	-42	43	24.04				-43 14073		11157	2
20289S4304	AOT 83	B	12.4	87.59	20	35	38.485	-42	43	27.12	112.12	8.172			11157	2	
20293S4208		A	12.3	87.59	20	35	58.762	-41	47	06.49				-42 14985		11157	2
20293S4208	AOT 84	B	12.5	87.59	20	35	59.903	-41	47	20.55	137.79	18.996			11157	2	
20302S2008		A	12.9	87.59	20	36	01.034	-19	47	36.79					11209	2	
20302S2008	AOT 85	B	14.1	87.59	20	36	00.474	-19	47	41.47	239.39	9.178			11209	2	
20303S4229		A	13.2	87.59	20	36	59.584	-42	08	07.87					11157	2	
20303S4229	AOT 86	B	14.0	87.59	20	36	59.147	-42	08	02.51	317.83	7.238			11157	2	
20307S4223		A	9.7	87.59	20	37	23.771	-42	02	17.87				-42 14995		11157	2
20307S4223	CPO 89	B	12.5	87.59	20	37	22.341	-42	02	13.66	284.80	16.472			11157	2	
20312S1955		A	13.2	87.59	20	36	55.037	-19	34	18.61					11209	2	
20312S1955	AOT 87	B	13.5	87.59	20	36	56.291	-19	34	36.21	134.79	24.981			11209	2	
20322S4314		A	10.8	87.59	20	38	54.232	-42	53	3.88				-43 14106		11157	2
20322S4314	AOT 88	B	14.3	87.59	20	38	55.336	-42	52	54.76	53.11	15.182			11157	2	
20329S1910		A	11.6	87.59	20	38	38.860	-18	48	30.07					11209	2	
20329S1910	AOT 89	B	14.3	87.59	20	38	39.346	-18	48	40.77	147.18	12.734			11209	2	
20336S1848	LEO 48	AB	10.7 11.6	87.59	20	39	16.465	-18	26	58.91				-18 5735		11209	2
20337S1909		A	13.8	87.59	20	39	23.213	-18	48	21.42					11209	2	
20337S1909	AOT 90	B	14.0	87.59	20	39	24.544	-18	48	26.97	106.37	19.706			11209	2	
20341S1848	RST3265	AB	11.1 11.1	87.59	20	39	48.857	-18	27	06.90				-18 5736		11209	2
20341S1848	HJ 2983	C	11.7	87.59	20	39	48.941	-18	27	22.87	175.73	16.014			11209	2	
20341S1939		A	13.3	87.59	20	39	51.615	-19	17	59.49					11209	2	
20341S1939	AOT 91	B	14.1	87.59	20	39	51.351	-19	18	17.02	192.05	17.921			11209	2	
20343S2001		A	13.9	87.59	20	40	01.423	-19	39	53.59					11209	2	
20343S2001	AOT 92	B	14.6	87.59	20	40	00.170	-19	39	51.32	277.29	17.857			11209	2	
20351S1922		A	13.0	87.59	20	40	49.587	-19	01	11.34				14137	11209	2	
20351S1922	BAR	B	13.6	87.59	20	40	49.279	-19	01	11.34	269.98	4.371		14137	11209	2	
20352S1852		A	13.8	87.59	20	40	56.306	-18	30	45.86					11209	2	
20352S1852	AOT 93	B	14.0	87.59	20	40	57.080	-18	31	01.75	145.29	19.328			11209	2	
20359S1949	RST3266	AB	10.5 11.4	87.59	20	41	36.955	-19	27	28.65				-19 5891		11209	2
20373S2003		A	12.4	87.59	20	43	00.776	-19	41	10.48					11209	2	
20373S2003	ARA1214	B	13.0	87.59	20	43	00.970	-19	41	06.69	35.90	4.681			11209	2	
20374S1940		A	13.4	87.59	20	43	07.958	-19	18	37.79					11209	2	
20374S1940	AOT 94	B	13.5	87.59	20	43	08.395	-19	18	46.38	144.20	10.590			11209	2	
20377S1950	HLD 40	CD	9.6 10.6	87.59	20	43	16.783	-19	29	32.97				-20 6014	14188	11209	2
20377S1950	HLD 40	AB	9.3 9.8	87.59	20	43	26.708	-19	28	57.41				-19 5901	14188	11209	2
20378S1928	HU 270	AB	9.8 10.3	87.59	20	43	30.516	-19	06	52.05				-19 5902	14191	11209	2
20378S1928		B	14.0	87.59										14191	11209	2	NS
20378S1928	AOT 95	D	12.2	87.59	20	43	32.688	-19	07	15.20	126.95	38.512			11209	2	
20563S1056		A	11.2	87.59	21	01	41.848	-10	32	18.62				-11 5500		11158	2
20563S1056	AOT 96	B	13.5	87.59	21	01	42.544	-10	32	21.42	105.27	10.643			11158	2	
20569S1003		A	9.1	87.59	21	02	20.836	-09	40	32.23				-10 5575		11158	2
20569S1003	HJ 929	B	10.0	87.59	21	02	20.790	-09	40	08.42	358.36	23.823			11158	2	
20572S1036		A	13.6	87.59	21	02	39.528	-10	12	13.36					11158	2	
20572S1036	AOT 97	B	14.1	87.59	21	02	39.592	-10	12	00.26	4.08	13.140			11158	2	
20575S1013		A	13.5	87.59	21	02	56.919	-09	49	47.14					11158	2	
20575S1013	AOT 98	B	13.7	87.59	21	02	55.880	-09	49	45.03	277.81	15.500			11158	2	
20578S0958		A	13.5	87.59	21	03	09.317	-09	34	44.55					11158	2	
20578S0958	AOT 99	B	14.2	87.59	21	03	09.745	-09	34	48.69	123.19	7.569			11158	2	
20580S1024		A	11.1	87.59	21	03	23.784	-09	59	49.31					11158	2	
20580S1024	AOT 100	B	14.1	87.59	21	03	24.590	-10	00	06.31	145.01	20.747			11158	2	



